

A solution of the Navier-Stokes differential equations

K. Shulev

An exact solution of the initial-boundary value problem for the complete Navier-Stokes differential equations, expressed in an explicit form, is derived. The problem corresponds to a viscous fluid flow induced by transverse motion of a long circular cylinder with a given initial speed.

Formulation of the problem

The complete Navier-Stokes equations of the form

$$(1) \quad \frac{\partial \bar{u}}{\partial t} + \text{rot } \bar{u} \times \bar{u} + \text{grad } \frac{u^2}{2} = -\frac{1}{\rho} \text{grad } p - \nu \text{rot } (\text{rot } \bar{u}), \quad \text{div } \bar{u} = 0,$$

in standard notations are considered. The problem is to find a solution of system (1) for \bar{u} and p , subject to boundary conditions at the initial instant $t=0$.

$$(2) \quad \bar{u}_s = \bar{U}, \quad \bar{u}_\infty = \bar{0}, \quad p_\infty = p_0,$$

where \bar{U} is the initial speed, s is the cylinder surface, p_0 is the pressure of resting fluid.

Solution

The cylinder motion is supposed to be along x direction, as the cylinder axis remains parallel to direction z of an absolute frame of reference. Suppose the flow to be in plane, in the cross plane to the cylinder axis xy . The components of $\text{rot } \bar{u} = \bar{\omega}(\omega_r, \omega_\theta, \omega_z)$ in cylindrical co-ordinates are

$$\omega_r = \frac{1}{r} \frac{\partial u_z}{\partial \theta} - \frac{\partial u_\theta}{\partial z}, \quad \omega_\theta = \frac{\partial u_r}{\partial z} - \frac{\partial u_z}{\partial r}, \quad \omega_z = \frac{1}{r} \left(\frac{\partial r u_\theta}{\partial r} - \frac{\partial u_r}{\partial \theta} \right),$$

so that the components of $\text{rot}(\text{rot } \bar{u}) = \text{rot } \bar{\omega} = \bar{\Omega}(\Omega_r, \Omega_\theta, \Omega_z)$ take the form

$$\Omega_r = \frac{1}{r} \frac{\partial \omega_z}{\partial \theta} - \frac{\partial \omega_\theta}{\partial z}, \quad \Omega_\theta = \frac{\partial \omega_r}{\partial z} - \frac{\partial \omega_z}{\partial r}, \quad \Omega_z = \frac{1}{r} \left(\frac{\partial r \omega_\theta}{\partial r} - \frac{\partial \omega_r}{\partial \theta} \right).$$

In case of polar co-ordinates in the plane xy then $u_z=0$, also $\frac{\partial(\circ)}{\partial z}=0$, consequently $\omega_r=0$, $\omega_\theta=0$. It follows in polar co-ordinates, that

$$\Omega_r = \frac{1}{r} \frac{\partial}{\partial \theta} \frac{1}{r} \left(\frac{\partial r u_\theta}{\partial r} - \frac{\partial u_r}{\partial \theta} \right), \quad \Omega_\theta = -\frac{\partial}{\partial r} \frac{1}{r} \left(\frac{\partial r u_\theta}{\partial r} - \frac{\partial u_r}{\partial \theta} \right), \quad \Omega_z = 0.$$

The system (1) in polar co-ordinates takes the form

$$(3) \quad \begin{aligned} \frac{\partial u_r}{\partial t} + \frac{1}{2} \frac{\partial}{\partial r} (u_r^2 + u_\theta^2) + \frac{u_\theta}{r} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) &= -\frac{1}{\rho} \frac{\partial p}{\partial r} + \nu \frac{\partial}{\partial r} \frac{1}{r} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) \\ \frac{\partial u_\theta}{\partial t} + \frac{1}{2r} \frac{\partial}{\partial \theta} (u_r^2 + u_\theta^2) - \frac{u_r}{r} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) &= -\frac{1}{\rho r} \frac{\partial p}{\partial \theta} - \nu \frac{\partial}{\partial r} \frac{1}{r} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) \\ \frac{\partial r u_r}{\partial r} + \frac{\partial u_\theta}{\partial \theta} &= 0. \end{aligned}$$

Applying rot in both sides of the first equation (1) it follows the system for the function \bar{u} only

$$(4) \quad \frac{\partial}{\partial t} \text{rot } \bar{u} + \text{rot} (\text{rot } \bar{u} \times \bar{u}) = -\nu \text{rot rot} (\text{rot } \bar{u}), \quad \text{div } \bar{u} = 0.$$

Such an elimination of pressure term is equivalent to cross differentiation of the first equation (3) with respect to θ , multiplying the second equation of (3) by r and differentiation with respect to r , by subtracting both equations. It follows the system

$$(5) \quad \begin{aligned} \frac{\partial}{\partial t} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) + \frac{\partial}{\partial \theta} \left[\frac{u_\theta}{r} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) \right] + \frac{\partial}{\partial r} \left(u_r \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) \right) \\ = \frac{\nu}{r} \frac{\partial^2}{\partial \theta^2} \frac{1}{r} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) + \nu \frac{\partial}{\partial r} r \frac{\partial}{\partial r} \left[\frac{1}{r} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) \right] \\ \frac{\partial r u_r}{\partial r} + \frac{\partial u_\theta}{\partial \theta} = 0 \end{aligned}$$

corresponding to system (4). The problem is then reduced to find a solution of system (5) subject to the following boundary conditions, at the initial instant $t=0$, when the cylinder axis coincides with axis z

$$(6) \quad u_r|_{r=a} = U \cos \theta, \quad u_\theta|_{r=0} = -U \sin \theta, \quad u_r|_{r=\infty} = 0, \quad u_\theta|_{r=\infty} = 0,$$

as $U = |U|$, a is the cylinder radius.

Introducing the stream function $\Phi(r, \theta, t)$

$$\Phi(r, \theta, t) = \psi(r, \theta) \exp\left(-\frac{\nu}{a^2} t\right)$$

through substitutions

$$u_r = \frac{1}{r} \frac{\partial \Phi}{\partial \theta}; \quad u_\theta = -\frac{\partial \Phi}{\partial r},$$

it follows that

$$(7) \quad u_r = \frac{1}{r} \frac{\partial \psi}{\partial \theta} \exp\left(-\frac{\nu}{a^2} t\right), \quad u_\theta = -\frac{\partial \psi}{\partial r} \exp\left(-\frac{\nu}{a^2} t\right).$$

Obviously the $\frac{\nu}{a^2} t$ is dimensionless variable, since the dimension of ν is $[\nu] = \frac{L^2}{T}$. Making use of (7) we obtain

$$(8) \quad \frac{1}{r} \left(\frac{\partial u_r}{\partial \theta} - \frac{\partial r u_\theta}{\partial r} \right) = \Delta \psi \exp\left(-\frac{\nu}{a^2} t\right)$$

where

$$(9) \quad \Delta\psi = \left(\frac{\partial^2}{\partial r^2} + \frac{1}{r} \frac{\partial}{\partial r} + \frac{1}{r^2} \frac{\partial^2}{\partial \theta^2} \right) \psi$$

is Laplace operator in polar co-ordinates. Substituting (7) and (8) into system (5) it follows the equation

$$(10) \quad -\frac{v}{a^2} \exp\left(-\frac{v}{a^2} t\right) r \Delta\psi + \left(\frac{\partial\psi}{\partial\theta} \frac{\partial\Delta\psi}{\partial r} - \frac{\partial\psi}{\partial r} \frac{\partial\Delta\psi}{\partial\theta} \right) \left[\exp\left(-\frac{v}{a^2} t\right) \right]^2 \\ = v \left(\frac{1}{r} \frac{\partial^2\Delta\psi}{\partial\theta^2} + \frac{\partial}{\partial r} r \frac{\partial\Delta\psi}{\partial r} \right) \exp\left(-\frac{v}{a^2} t\right).$$

On the other hand we have

$$\frac{\partial}{\partial r} r \frac{\partial\Delta\psi}{\partial r} + \frac{1}{r} \frac{\partial^2\Delta\psi}{\partial\theta^2} = r \frac{\partial^2\Delta\psi}{\partial r^2} + \frac{\partial\Delta\psi}{\partial r} + \frac{1}{r} \frac{\partial^2\Delta\psi}{\partial\theta^2} = r \left(\frac{\partial^2\Delta\psi}{\partial r^2} + \frac{1}{r} \frac{\partial\Delta\psi}{\partial r} + \frac{1}{r^2} \frac{\partial^2\Delta\psi}{\partial\theta^2} \right) = r \Delta\Delta\psi,$$

so that the equation (10), after reduction $\exp\left(-\frac{v}{a^2} t\right)$, takes the form

$$(11) \quad \left(\frac{\partial\psi}{\partial\theta} \frac{\partial\Delta\psi}{\partial r} - \frac{\partial\psi}{\partial r} \frac{\partial\Delta\psi}{\partial\theta} \right) \exp\left(-\frac{v}{a^2} t\right) = vr \Delta \left(\Delta\psi + \frac{\psi}{a^2} \right).$$

It is readily shown that

$$(12) \quad \Delta\psi = -\frac{\psi}{a^2}$$

satisfy the equation (11), and this being so, a solution of equation (11) may be derived from the solutions of equation (12). It follows from (7) at the initial instant $t=0$ that

$$(13) \quad u_r = \frac{1}{r} \frac{\partial\psi}{\partial\theta}, \quad u_\theta = -\frac{\partial\psi}{\partial r}.$$

In such a way the stated initial-boundary value problem is reduced to the boundary problem in finding a solution of equation (12), subject to boundary conditions (6) through substitutions (13). This problem already has been solved in [1] or [2], which is, in the same time, a solution of the Euler differential equations subjected to no-slip boundary condition at the cylinder surface. In this case the stream function has the form

$$\psi(r, \theta) = Uaf\left(\frac{r}{a}\right) \sin\theta,$$

where $f\left(\frac{r}{a}\right) = f(\xi)$ is determined as solution of Bessel equation

$$f'' + \frac{1}{\xi} f' + \left(1 - \frac{1}{\xi^2}\right) f = 0.$$

The general solution is

$$f\left(\frac{r}{a}\right) = AJ_1\left(\frac{r}{a}\right) + BN_1\left(\frac{r}{a}\right),$$

where $J_1\left(\frac{r}{a}\right)$ and $N_1\left(\frac{r}{a}\right)$ are standard Bessel functions. The constants of integration A and B are to be determined from the first two boundary conditions (6) which leads to the system

$$(14) \quad \begin{aligned} AJ_1(1) + BN_1(1) &= 1 \\ AJ_1'(1) + BN_1'(1) &= 1 \end{aligned}$$

with the solution

$$A = \frac{\pi}{2} [N_1'(1) - N_1(1)], \quad B = -\frac{\pi}{2} [J_1'(1) - J_1(1)].$$

As it is easily verified, the last two conditions of (6) are satisfied too, because the functions $J_1(\xi)$, $J_1'(\xi)$, $N_1(\xi)$ and $N_1'(\xi)$ tend to 0 as $\xi \rightarrow \infty$. The solution then for u and u for the initial instant $t=0$ is

$$(15) \quad \begin{aligned} u_r(r, \theta) &= \frac{U\pi a}{2r} \left[A J_1\left(\frac{r}{a}\right) + B N_1\left(\frac{r}{a}\right) \right] \cos \theta \\ u_\theta(r, \theta) &= -\frac{U\pi}{2} \left[A J_1'\left(\frac{r}{a}\right) + B N_1'\left(\frac{r}{a}\right) \right] \sin \theta. \end{aligned}$$

Then the solution of the stated initial boundary-value problem for u_r and u_θ for each $t \geq 0$, in view of (7), is

$$(16) \quad \begin{aligned} u_r(r, \theta, t) &= \frac{U\pi a}{2r} \left[A J_1\left(\frac{r}{a}\right) + B N_1\left(\frac{r}{a}\right) \right] \cos \theta \cdot \exp\left(-\frac{v}{a^2} t\right) \\ u_\theta(r, \theta, t) &= -\frac{U\pi}{2} \left[A J_1'\left(\frac{r}{a}\right) + B N_1'\left(\frac{r}{a}\right) \right] \sin \theta \cdot \exp\left(-\frac{v}{a^2} t\right). \end{aligned}$$

It is obvious that the solution (16) is subjected to the following boundary conditions for each $t \geq 0$:

$$(17) \quad \begin{aligned} u_r|_{r=a} &= U \cos \theta \cdot \exp\left(-\frac{v}{a^2} t\right), \quad u_\theta|_{r=a} = -U \sin \theta \cdot \exp\left(-\frac{v}{a^2} t\right) \\ u_r|_{r=\infty} &= 0, \quad u_\theta|_{r=\infty} = 0. \end{aligned}$$

The first two conditions (17) can be written in the following vector form

$$(18) \quad \bar{u}_s = \bar{U} \exp\left(-\frac{v}{a^2} t\right).$$

Due to $v > 0$, it is evident from (18), that the cylinder makes delaying motion subjected to exponential law. In case $v=0$ the cylinder motion becomes uniformly one with constant speed \bar{U} .

Integrating system (3) and determining the constant of integration from the condition $p_\infty = p_0$ follows the pressure distribution $p(r, \theta, t)$. We give the final result as

$$p(r, \theta, t) = p_0 - \frac{\rho}{2} \left(u_r^2 + u_\theta^2 - \frac{\Phi^2}{a^2} \right),$$

where u_r and u_θ are given by (16) while

$$\Phi(r, \theta, t) = Ua \left[A J_1\left(\frac{r}{a}\right) + B N_1\left(\frac{r}{a}\right) \right] \sin \theta \cdot \exp\left(-\frac{v}{a^2} t\right).$$

In such a way the stated initial-boundary value problem has completely been solved.

The stated problem allows a generalization by extension of the initial boundary conditions (6) to the following

$$u_r|_{r=a} = U\alpha \cos \theta, \quad u_\theta|_{r=a} = -U\beta \sin \theta, \quad u_r|_{r=\infty} = 0, \quad u_\theta|_{r=\infty} = 0,$$

where α and β are dimensionless parameters. Then the system determining the constants A and B , which corresponds to the system (14) is

$$\begin{aligned} A J_1(1) + B N_1(1) &= \alpha \\ A J_1'(1) + B N_1'(1) &= \beta. \end{aligned}$$

The above system always has unique solution. In case $\alpha=1$, $\beta=1$ follows boundary conditions (6), but when $\alpha \neq 1$, $\beta \neq 1$ they become disturbed. In specific case $\alpha=1$, and β could be arbitrarily chosen following boundary condition of inviscid fluid. This being so it is significant that the Navier-Stokes differential equations could have vortex solution subject to boundary conditions of inviscid fluid.

It is worth also noticing that the solution derived here has the essential property when $v \rightarrow 0$ then the solution tends to the solution of the Euler differential equations subject to boundary condition of viscous fluid, with no-slip condition at the cylinder surface. In the light of this fact the Oseen's concept, concerning the impossibility Euler equation solution to be derived, in the particular case $v=0$, from Navier-Stokes equation solution [3], needs a revision.

References:

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